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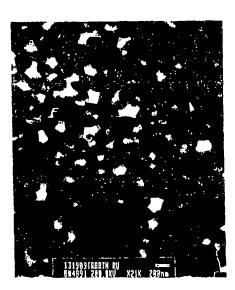
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(54) Title: GRAFT COPOLYMERS OF METHYLENE LACTONES AND PROCESS FOR EMULSION POLYMERIZATION OF METHYLENE LACTONES



(57) Abstract: This invention discloses resilient, acrylic graft polymers comprising α-methylene lact(one)(am) monomers such as α-methylene-y-butyrolactone, and blends of such polymers with thermoplastic matrix resins. This invention also discloses hard, non-resilient, acrylic graft polymers comprising α-methylene lact(one)(am) monomers such as α-methylene-γ-butyrolactone, and to blends of such polymers with thermoplastic matrix resins. This invention further discloses a general process for emulsion polymerization of α-methylene lact(one)(am) monomers such as α-methylene-γ-butyrolactone and its copolymers.

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TITLE

GRAFT COPOLYMERS OF METHYLENE LACTONES AND PROCESS FOR EMULSION POLYMERIZATION OF METHYLENE LACTONES

FIELD OF THE INVENTION

This invention relates to resilient, acrylic graft polymers derived from α -methylene lact-(ones)(ams) such as α -methylene- γ -butyrolactone (MBL), and to blends of such polymers with thermoplastic matrix resins.

This invention also relates to hard, nonresilient, acrylic graft polymers derived from α -methylene lact(ones)(ams) such as α -methylene- γ -butyrolactone (MBL), and to blends of such polymers with thermoplastic matrix resins.

This invention further relates to a general process for emulsion polymerization of α -methylene lact(ones)(ams) such as α -methylene- γ -butyrolactone (MBL) and its copolymers.

BACKGROUND OF THE INVENTION

Resilient, acrylic graft polymers are produced by a multi-stage, sequential polymerization technique which comprises alternately producing resilient and nonresilient layers around an acrylic core material. Such materials are often referred to as "core/shell particles" or "core/shell tougheners". These resilient polymers are ordinarily mixed with a hard nonresilient thermoplastic methacrylic matrix resin in order to provide toughness in articles molded from the resulting blend. When properly dispersed, the resilient acrylic graft polymer greatly improves the impact strength of the hard matrix resin while maintaining a balance of important physical properties of heat distortion temperature, flexural modulus, tensile strength and tensile elongation.

A number of patents and papers address polymer morphology that can be obtained by multi-stage emulsion polymerization. For a detailed discussion, see P. Lovell, M. El-Aasser *Emulsion Polymerization and Emulsion Polymers*, John Wiley and Sons, 1997, chapter 19. See also U.S. Patents 5,625,001 and 5,998,554, 3,678,133, 3,793,402, 3,808,180, 3,985,703, 4,180,494, 4,543,383 and World Patent Application 99/12986. The above art provides a description of monomers, emulsifiers, graft-linking monomers, cross-linking monomers, initiators, and the like, useful in making staged (meth)acrylic emulsion polymers.

Polymeric MBLs are characterized by high glass transition temperatures, but are often quite brittle. See for instance U.S. Patent 5,880,235 and the discussion at columns 1-3, and D. Arnoldi, et al., Kunststoffe, vol. 87, p. 734-736 (1997). Commercially available acrylic graft copolymers, such as the Paraloid[®] series of products sold by Rohm and Haas Co., Philadelphia, PA, U.S.A., can be used to toughen MBL-containing polymers. However, an important criterion for toughening is the compatability of the shell of the core/shell particle with the matrix polymer. Poor compatibility leads to particle agglomeration, which results in poor physical properties in the resulting molded product. Thus, if one could use multistage graft copolymers derived from MBLs to toughen matrix resins containing MBLs without compromising their other superior properties, useful compositions would result. In addition, functional groups can be incorporated in the outer shell of the MBLcontaining graft copolymer to improve compatibility with other thermoplastic polymers such as polyolefins, polyamides, polyesters, polycarbonates, polystyrenes, ABS-type polymers, polyacetals, polyethers, polyurethanes, poly(vinyl chloride), blends thereof and mixtures thereof.

Another aspect of the present invention is a process for preparing hard, nonresilient, cross-linked polymers from MBLs. These polymers have a fixed particle size and act as nano-sized (less than about 500 nanometer), pre-formed, high glass transition temperature (T_g) amorphous "filler" materials. When properly blended with thermoplastic resins, the resulting materials display much higher heat distortion temperatures than the thermoplastic alone.

This invention further discloses an emulsion polymerization process of preparing MBL-based homopolymers and copolymers. A general emulsion polymerization process is described in "Polymer Chemistry," by Seymour and Carraher, fifth edition, Marcel Dekker, Inc. NY, 2000 and "Introduction to Polymers," Young and Lovell, second edition, Chapman & Hall, 1991.

US 3,444,148 to Adelman in Example 10 teaches synthesis of a 1/6 (w/w) γ , γ -bis-trifluromethyl MBL/acrylonitrile copolymer via emulsion polymerization. However, there is no teaching for synthesis of higher MBL content copolymers and MBL homopolymers via emulsion polymerization. The distinctive feature of emulsion polymerization is the ease with which comonomer ratios can be adjusted during the reaction. For a detailed discussion, see C. B. Bucknall, *Toughened Plastics*, Applied

Science Publishers, 1977, p. 99. In addition, the heats of reaction, particle size, molecular weight, and molecular weight distribution can be carefully controlled. Within the scope of the present invention, the MBL core/shell latex can be easily mixed with the MBL copolymer latex in the desired ratio and then coagulated together. Although this is commonly done, for example, in the manufacture of acrylonitrile/butadiene/styrene based polymers via emulsion, (see P. Lovell, M. El-Aasser *Emulsion Polymerization and Emulsion Polymers*, John Wiley and Sons, 1997, p. 668-670), the process has never been suggested for the preparation of MBL-based homopolymers and copolymers.

Among the uses of thermoplastics are those in which the optical properties of the polymer are important, particularly when the polymer is an optically clear material with little distortion of optical images. Such polymers, for example poly(methyl methacrylate) (PMMA) and certain polycarbonates are used as substitutes for glass where toughness is important, such as for safety glazing and signage. In uses where toughness is important, additional properties such as weather and/or heat resistance may also be important. For example, if a material needs to be thermally sterilized, it must withstand the temperature of the sterilization process. Polycarbonates often have poor weathering and/or hydrolysis resistance, while PMMA has a relatively low glass transition temperature (T_g), so its heat resistance is poor. Thus, polymers with a combination of good optical properties, and heat and weathering resistance are desired.

An important criterion for optical clarity is that the refractive index (RI) of the acrylic graft copolymer match that of the matrix thermoplastic to within 0.1% of refractive index units. This can be done by adjusting the ratio of styrene (RI of 1.590) to n-butyl acrylate (RI of 1.466) in the rubbery phase of the acrylic graft copolymer. While this technique is common to PMMA (RI 1.490), it has not yet been demonstrated with polymers of MBL (RI of 1.540) or polymers of γ -methyl MBL (RI of 1.510). The present invention teaches a process for making transparent polymer compositions can be obtained from multi-stage graft copolymer blends of MBL and γ -methyl-MBL (Me-MBL).

The acrylic-copolymers and compositions of the invention are of use as molded parts, thermoform parts, sheets, films, foams, containers, bottles, pipes, profiles and other articles made in accordance with the invention.

SUMMARY OF THE INVENTION

The invention relates to an acrylic copolymer comprising at least a first polymeric repeat unit represented by Formula I, derived from α -methylene lact(one)(am) monomer,

$$H_2C$$
 R^1
 R^2
 R^3
 R^4
 R^5
(I)

wherein:

n is 0, 1 or 2;

X is -O- or -NR9-; and

R¹, R², R⁵, R⁶, R⁹, each of R³, and each of R⁴, are independently hydrogen, a functional group, hydrocarbyl or substituted hydrocarbyl.

The invention also relates to a process for producing an acrylic copolymer comprising the sequential steps of:

- (a) graft polymerizing α -methylene- γ -butyrolactone or γ -methyl- α -methylene- γ -butyrolactone onto a polymerized butadiene or butadiene-copolymer to form a latex, and
- (b) isolating the resulting latex by coagulation, freeze drying, or spray drying.

 BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a TEM analysis of a film of MeMBL core/shell particles from Example 13.

Figure 2 is a TEM analysis of NBA/Styrene // MeMBL/MMA core//shell particles corresponding to Example 23.

Figure 3 is a TEM analysis of the polymer blend from Example 25 showing good dispersion of the MBL-MMA core/shell particles in the MBL-MMA copolymer matrix.

DETAILED DESCRIPTION OF THE INVENTION

The terms used in the present invention are defined below.

The term " α -methylene lact(ones)(ams)" as used herein refers to monomers of α -methylene lactones and monomers of α -methylene lactams. The polymers of the present invention can comprise either one or both monomers of α -methylene lactones and monomers of α -methylene lactams.

A "hydrocarbyl group" is a univalent group containing only carbon and hydrogen. If not otherwise stated, it is preferred that hydrocarbyl groups (and alkyl groups) herein contain 1 to about 30 carbon atoms.

By "substituted hydrocarbyl" herein is meant a hydrocarbyl group which contains one or more substituent groups which are inert under the process conditions to which the compound containing these groups is subjected. The substituent groups also do not substantially interfere with the process. If not otherwise stated, it is preferred that substituted hydrocarbyl groups herein contain 1 to about 30 carbon atoms. Included in the meaning of "substituted" are heteroaromatic rings. In substituted hydrocarbyl all of the hydrogens may be substituted, as in trifluoromethyl.

By "functional group" herein is meant a group other than hydrocarbyl or substituted hydrocarbyl which is inert under the process conditions to which the compound or polymer containing the group is subjected. The functional groups also do not substantially interfere with any process described herein that the compound or polymer in which they are present may take part in. Examples of functional groups include halo (fluoro, chloro, bromo and iodo), ether such as -OR²² wherein R²² is hydrocarbyl or substituted hydrocarbyl.

By "reactive functional group" is meant a functional group that may react with another functional group present in the process or composition. By "may react" is meant that the functional group may react with its counterpart reactive group, but it is not necessary that such reaction happen or that all of the reactive functional groups react with one another. Usually in the formation of the compositions described herein, some fraction of these reactive functional groups will react.

By "derived from" is meant that the polymer is prepared from the monomers set forth in the particular embodiment as commonly known and referred to by persons skilled in the art.

By "copolymerizable under free radical conditions" is meant that the (potential) monomers, preferably vinyl monomers, involved are known to copolymerize under free radical polymerization conditions. The free radicals may be generated by any of the usual processes, for example thermally from radical initiators such as peroxides or azonitriles, by UV-radiation using appropriate sensitizers, etc., and by ionizing radiation. These polymers may be prepared by various types of processes, such as continuous, batch, and semibatch, which are well known in the art. Many combinations of free radically copolymerizable monomers are known, see for instance, J. Brandrup, et al., Ed., Polymer Handbook, 4th Ed., John Wiley & Sons, New York, 1999, p. II/181-II/308.

By "an elastomeric or rubbery polymer" is meant a polymer having a flexural modulus (of unfilled pure elastomeric polymer) of 35 MPa or less as measured by the ASTM D790 method, and having a T_g of less than 30°C, preferably having a T_g of less than 0°C. Glass transition temperatures are measured by the ASTM D3418 method at a heating rate of 20°C/min. The T_g is measured as the midpoint of the transition of the glass transition temperature.

By "batch emulsion polymerization" is meant that all ingredients, including monomers, surfactants, and chain transfer agents, are added at the beginning of the polymerization. The polymerization begins as soon as initiator is added.

By "semi-continuous emulsion polymerization" is meant that one or more of the ingredients is added continuously or in incremental amounts. The monomers may be added in pure form or as pre-made emulsions. This process is advantageous over the batch process by allowing better control over heat of reaction, particle number, colloidal stability, coagulum formation, and particle morphology.

By "continuous emulsion polymerization" is meant that one or more ingredients is fed continuously to a polymerization tank or series of tanks and the polymer product (latex) is continuously removed at the same rate. By "low-temperature emulsion polymerization" is meant that emulsion polymerization reaction is carried out with a redox-type initiator.

Optionally, cross-linked homopolymers based on repeating units of α -methylene lact(one)(am) (of Formula II), are herein prepared by emulsion polymerization,

$$H_2C$$
 R^1
 R^2
 R^3
 R^4
 R^5
(II)

wherein:

n is 0, 1 or 2;

X is -O- or -NR9-; and

R¹, R², R⁵, R⁶, R⁹, each of R³, and each of R⁴, are independently hydrogen, a functional group, hydrocarbyl or substituted hydrocarbyl.

Optionally, cross-linked copolymers based on repeat units of α -methylene lact(one)(am) (Formula II) are also herein prepared by emulsion polymerization.

Optionally, cross-linked copolymers wherein at least one repeat unit is α -methylene lact(one)(am) (Formula II) and at least one other repeat unit is a free-radically polymerizable monomer, are also prepared by emulsion polymerization. Preferably, the free-radically polymerizable monomer-based repeat units have the following Formulae:

$$R^{16}$$
 R^{16}
 R^{17}
 R^{18}
 R^{19}
 R^{18}
 R^{19}
 R^{19}
 R^{18}

$$0 = C \qquad C = 0$$

$$OR^{23} \qquad OR^{24}$$

VII (cis structure)

$$\begin{array}{c|c}
O \\
C \\
C \\
C \\
C
\end{array}$$

$$\begin{array}{c|c}
O \\
C \\
C \\
C
\end{array}$$

$$\begin{array}{c|c}
O \\
C \\
C \\
C
\end{array}$$

VIII (trans structure)

wherein R^{14} is hydrogen or methyl, and R^{15} is hydrocarbyl or substituted hydrocarbyl, preferably alkyl, and R^{16} is hydrogen or methyl and R^{17} , R^{18} , R^{19} ,

R²⁰ and R²¹ are each independently hydrogen, hydrocarbyl substituted hydrocarbyl or a functional group. In a preferred embodiment of the compound of Formula (V), R¹⁴ and R¹⁵ are both methyl (methyl methacrylate), and in a preferred embodiment of the compound of Formula (VI), R¹⁶, R¹⁷, R¹⁸, R¹⁹, R²⁰ and R²¹ are all hydrogen (styrene), and R²³, R²⁴, R²⁶, and R²⁷ are methyl, ethyl or butyl.

Multi-stage, core/shell polymeric particles are herein prepared by the process of emulsion polymerization. In this process, each successive stage is polymerized in the presence of previously formed stages. Thus, each successive stage is polymerized as a layer on top of the immediately preceding stage. Depending on the properties desired, the first stage may comprise a seed surrounded by more first stage. Thus, the first stage or the portion of the first stage is used as a seed or "core", around which either more of the first stage or the subsequent stages known as shells are polymerized in layers. The first stage or a portion thereof, which forms the core provides a mechanism for determining final particle size; for once the core particles are formed, subsequent polymerization of the stage tends to result in polymerization on the existing particles, i.e., generally new particles do not form. Thus, the final particle size is controlled by the number of first stage core particles.

A preferred embodiment of a multi-stage, core/shell particle consists of a core and two shells. The inner shell is known as the intermediate layer.

The multi-stage, sequentially produced polymer herein comprises repeat units derived from the monomer represented by Formula (II) above.

In particularly preferred embodiments of compounds of Formula (II), n is 0, X is -O- and R^1 , R^2 , R^5 and R^6 are hydrogen, or n is 0, X is -O-, R^6 is methyl, and R^1 , R^2 and R^5 are hydrogen. Other preferred embodiments of compounds of Formula (II) are set forth in U.S. Patent 5,880,235, which is hereby incorporated by reference, at column 4, line 44 to column 8, line 59.

A free radically polymerizable monomer may also be present in the multistage, sequentially produced polymer. Preferably these repeat units are derived from monomers of Formulae (V) and (VI) above.

In a preferred embodiment of the compound of Formula (V), R^{14} and R^{15} are both methyl (methyl methacrylate), and in a preferred embodiment of the compound of Formula (VI), R^{16} , R^{17} , R^{18} , R^{19} , R^{20} and R^{21} are all hydrogen (styrene).

The core of the core/shell multi-stage polymeric particle may be cross-linked and is a polymer selected from:

- (a) a polymer or a copolymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula I above,
- (b) a polymer or a copolymer derived from at least one other free-radically polymerizable monomer of Formula (V) or Formula (VI) above,
- (c) a copolymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula II and at least one other free-radically copolymerizable monomer,
- (d) an optionally cross-linked polymer derived from at least one conjugated diolefin monomer,
- (e) an optionally cross-linked polymer derived from at least one vinyl monomer, and
- (f) an optionally cross-linked polymer derived from at least one conjugated diolefin monomer and one vinyl monomer.

The shell of the core/shell multi-stage polymeric particle may be cross-linked and is a polymer selected from:

- (a) a polymer or a copolymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula II above,
- (b) a polymer or a copolymer derived from at least one other free-radically polymerizable monomer of Formula (V) or Formula (VI) above,
- (c) a copolymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula II and at least one other free-radically copolymerizable monomer,
- (d) an optionally cross-linked polymer derived from at least one conjugated diolefin monomer,
- (e) an optionally cross-linked polymer derived from at least one vinyl monomer, and
- (f) an optionally cross-linked polymer derived from at least one conjugated diolefin monomer and one vinyl monomer.

If the multi-stage sequential polymer comprises of an intermediate layer, the intermediate layer comprises a polymer selected from:

(a) a polymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula II,

- (b) a polymer derived from at least one free radically polymerizable monomer,
- (c) a copolymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula II and at least one other free radically polymerizable monomer,
- (d) an optionally cross-linked polymer, derived from at least one conjugated diolefin monomer,
- (e) an optionally cross-linked polymer, derived from at least one vinyl monomer, and
- (f) an optionally cross-linked polymer derived from at least one conjugated diolefin monomer and one vinyl monomer.

The resilient, acrylic graft polymers derived from α -methylene lact(ones)(ams) such as α -methylene- γ -butyrolactone (MBL), are blended with thermoplastic matrix resins in this invention. The non-resilient, acrylic graft polymers derived from α -methylene lact(ones)(ams) such as MBL, are also blended with thermoplastic matrix resins in this invention. A thermoplastic resin based on a polymer or copolymer of α -methylene lact(ones)(ams) such as MBL is preferred for the blending.

A homopolymer or copolymer derived from MBL monomer and the methyl methacrylate monomer is preferred as the matrix resin for blending. The weight fraction of MBL in the copolymer ranges from 0% to 100%. The number average molecular weight of the homopolymer or copolymer ranges from about 5,000 to about 100,000. More preferably, the number average molecular weight of the homopolymer or copolymer ranges from about 40,000 to about 70,000.

Polyamide resin is also preferred as the matrix resin for blending with multistage polymeric particles prepared by this invention. Polyamides useful for compositions of this invention include conventional polyamide resins known as nylon resins, including both aliphatic polylactams such as polycaprolactam (nylon 6) and higher analogs such as nylon 11 and nylon 12, and polyamides formed from aliphatic diamines and aliphatic dicarboxylic acids such as polyhexamethylene sebacamide (nylon 6,10) polyhexamethylene adipamide (nylon 6,6), and the like. Further examples of useful polyamides include the amorphous as well as the crystalline versions, the toughened polyamides, and the aromatic-aliphatic copolymers,

terpolymers and tetrapolymers. A great variety of these nylon resins are well known and widely available commercially.

Cross-linked, multi-stage particles are preferred for addition to polyamide resin. Preferably, cross-linked particles of MBL homopolymer, MBL copolymer with methacrylic acid, MBL copolymer with methacrylamide, MBL copolymer with itaconic anhydride, or MBL copolymer with maleic anhydride are used as impact modifiers for the polyamide resin.

Combining the multi-stage polymeric particles and thermoplastic polymeric resins may be accomplished by any of the common melt-blending processes, including the use of compounding extruders, Banbury mixers, roll mills, and the like. The powdered or pelletized resins may be dry-blended, then fed to the processing equipment, or alternatively, the resinous components may be fluxed in the melt processing equipment, with subsequent addition of multi-stage impact modifiers.

Generally the graft polymers or the multi-stage polymers are present in an amount of about 1% to about 80% by weight of the blend, preferably from about 30% to about 70%, and more preferably from about 55% to about 65%.

The final particle size of the multistage core/shell particle prepared by the method of this invention is between about 100 nanometer to about 500 nanometer, and more preferably from about 200 to about 300 nanometer.

A preferred core weight content range is from about 10% to about 90% of the total weight of the multiphase polymeric particle. A more preferred core weight content range is from about 20% to about 80%. A further preferred core weight content range is from about 20% to about 30%.

A preferred intermediate shell weight content range is from 0 % to about 60% of the total weight of the multiphase polymeric particle. A more preferred intermediate shell weight content range is from about 35% to about 65%. A most preferred intermediate weight content range is from about 45% to about 55%.

A preferred outer shell weight content range is from about 0 % to about 35% of the total weight of the multiphase polymeric particle. A more preferred outer shell weight content range is from about 5% to about 30%. A further preferred outer weight content range is from about 15% to about 25%.

Emulsion polymerization temperatures can range from 25°C to about 100°C, preferably from about 60°C to about 80°C.

Preferred initiators for the polymerization process include thermal type initiator systems. Examples of thermal initiators include organo peroxides, acetyl peroxides, lauroyl peroxide, t-butyl peroxide, di-t-butyl hydroperoxide, peresters, such as t-butyl peroxypivulates; azo-type initiators, such as azo-bis-isobutyrylnitrile; persulfates, such as sodium, potassium, or ammonium persulfate; and peroxyphosphastes, such as sodium, potassium, or ammonium peroxyphosphate.

Preferred initiators for the polymerization process also include redox-type initiator systems. Redox initiators include, for example, a combination of a hydroperoxide, such as hydrogen peroxide, t-butyl hydroperoxide, cumene hydroperoxide, diisopropyl-benzene hydroperoxide, and the like, and a reducing agent, such as sodium, potassium, or ammonium bisulfite, metabisulfite, or hydrosulfite, sulfur dioxide, hydrazine, ferrous salts, isoascorbic acid, and sodium formaldehyde sulfoxalate.

Suitable surfactants for the polymerization process include alkali metal, ammonium salts of alkyl, aryl, alkaryl, ara-alkyl sulfonates, sulfates and polyether sulfates, ethoxylated fatty acids, esters, alcohols, amines, amides, alkyl phenolics, complex organo-phosphoric acids, and their alkali metal and ammonium salts.

Suitable chain transfer agents for the emulsion polymerization process include mercaptans, polymercaptans, and polyhalogen compounds.

Suitable coagulants for the emulsion polymerization process includes magnesium sulfate, sodium chloride and calcium chloride.

All of the compositions herein may additionally comprise other materials commonly found in thermoplastic compositions, such as lubricants, fillers, reinforcing agents, dyes, pigments, antioxidants, and antiozonants. They may also include the addition of polymer to modify the impact strength such as Fusabond® EPDM rubbers, Surlyn® ethylene copolymers, Kraton® rubbers, Elvaloy® ethylene copolymers and the like. These materials may be present in conventional amounts, which vary according to the type(s) of material(s) being added and their purpose in being added.

EXAMPLES AND COMPARATIVE EXAMPLES

The present invention is further defined in the following examples, in which all parts and percentages are by weight and degrees are Celsius, unless otherwise stated. It should be understood that these examples, while indicating preferred em-

PRISOCCIO: 4MO

bodiments of the invention, are given by way of illustration only. From the above discussion and these examples, one skilled in the art can ascertain the essential characteristics of this invention, and without departing from the spirit and scope thereof, can make various changes and modifications of the invention to adapt it to various usage and conditions.

In the Examples, the following abbreviations are used:

GPC - gel permeation chromatography

PD - polydispersity index

MBL - α-methylenebutyrolactone

MeMBL - γ -methyl- α -methylenebutyrolactone

MMA - methyl methacrylate

Mn - number average molecular weight

Mw - weight average molecular weight

PD - polydispersity index

T_g - glass transition temperature (20°C/min. heating rate)

T_d - onset of decomposition temperature (20°C/min. heating rate)

NBA - n-butyl acrylate

DOS - sodium dioctylsulfosuccinate surfactant

Alma - allyl methacrylate

K₂S₂O₈ - potassium persulfate initiator

EHT- 2-ethylhexylthioglycolate chain transfer agent

GMA - glycidyl methacrylate

HEMA - hydroxyethyl methacrylate

EMA - ethyl methacrylate

CHMA - cyclohexyl methacrylate

BMA - butyl methacrylate

MAAM - methacrylamide

MAN - maleic anhydride

RI - refractive index

EDTA - ethylene diamine tetracetic acid

Common reagents were obtained from Aldrich Chemical Co., Milwaukee, WI,

U.S.A. Paraloid® toughener was obtained from Rohm & Haas Co., Philadelphia, PA,

U.S.A. The molecular weight was determined by triple detector GPC with 2

Showdex[®] 80M columns, a Waters[®] 410 RI detector and a Viscofek[®] T60A light scattering and viscometry detector. The solvent was hexafluoroisopropanol and 0.01 M sodium triflate as the solvent using Zytel[®] 101 as a standard. Zytel[®] 101 was obtained from E.I. du Pont de Nemours & Co., Wilmington, DE.

Polymer blending was carried out with a 16 mm twin screw extruder, Welding Engineers Model TSE 16TC with a 3.2 mm die and 60 kPa of vacuum on port no. 3, and was operated at 250 rpm. Glass transition temperatures were measured by ASTM D3418 at a heating rate of 20°C/min and the T_g measured as the midpoint of the transition. Notched Izod testing was carried out according to ASTM D256 on specimen about 0.1250.3175 cm thick. The flexural modulus was measured by ASTM D790. The tensile percent elongation was measured according to ASTM D638. Heat deflection temperature was determined according to ASTM D648 at 1.82 MPa load.

Transmission Electron Microscopy (TEM) was carried by sectioning molded plaques or pieces by cryo-ultramicrotomy. Sections of a nominal thickness 90 nanometer were accumulated in cold ethanol, transferred to water and retrieved on copper mesh grids. Images were obtained using a JEOL 1200 EX TEM operated at 100 KV accelerating voltage and recorded on sheet film.

EXAMPLE 1

Preparation of MBL Homopolymer by Emulsion Polymerization

Step 1: Preparation of MBL seed polymer

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 2.7L water and sparged with nitrogen for 30 min. A solution of MBL (150g), EHT (0.58g), and DOS (1.36g, 0.003 mol) was added and the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.165g) in 35mL water was added over 5 min. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky-white emulsion. The mixture was allowed to stir at 80°C for 1 hour.

Step 2: Addition of MBL

A solution of potassium persulfate (0.39g) in 150mL water was added over 5 min to the milky-white emulsion obtained from step 1. A solution of MBL (400g), EHT (1.6g), and DOS (3.62g) was added over 1 hour and then held for 1 hour at 80°C.

Step 3: Coagulation of MBL homopolymer

See example 10 for coagulation of MBL homopolymer.

EXAMPLE 2

Preparation of 1/1 MBL-MMA Copolymer by Emulsion Polymerization

Step 1: Preparation of MBL-MMA seed polymer

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 2.7 L water and sparged with nitrogen for 30 min. A solution of MBL (75g), MMA (75g), EHT(0.73g), and DOS (1.36g) was added and the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.155g) in 35mL water was added over 5 minutes. Polymerization began immediately and the mixture turned from a cloudy clear emulsion to a milky white emulsion. The mixture was allowed to stir at 80°C for 1 hour.

Step 2: Addition of MBL and MMA monomer

A solution of potassium persulfate (0.39g) in 75mL water was added over 5 min to the cloudy emulsion mixture obtained from step 1. A solution of MBL (200g), MMA (200g), EHT(2.06g), and DOS(3.62g) was added over 1 hour, and then held for 1 hour at 80°C.

Step 3: Coagulation of MBL-MMA copolymer

The polymer emulsion (from Step 2) was allowed to cool to room temperature and filtered through course frit filter paper. The emulsion was coagulated with 12L of a 1% MgSO₄ solution at 100°C. The slurry was allowed to cool and polymer was collected on a course frit filter and washed with water three times with 2L of water each time and dried to give 534g (97%) of the MBL-MMA copolymer as a white solid. The polymer had the following properties:

TABLE 1

Property		Comments
T _g	144°C	measured by DSC at 20°C/min heating
		rate
Tå	376°C	measured by DSC at 20°C/min heating
		rate
Mn	59,500	measured by triple detector GPC
Mw	146,00	measured by triple detector GPC
	0	
PD=(Mw/Mn)	2.4	

EXAMPLES 3-9

Using the general procedure described in Example 2, the following copolymers were prepared by emulsion polymerization of MBL.

TABLE 2

								
Example	Composition	Weight	Yield(%)	Tg	T _d	Mn	Mw	PD
No.		Ratio		°C ·	°C			
3	MBL/EMA	1/1	97	121	367	43,500	127,200	2.9
4	MBL/CHMA	1/1	88	147	264	57,000	190,000	3.3
5	MBL/Styrene	1/1	95	154	392	43,100	168,000	3.9
6	MBL/NBMA	1/1	95	85	354	51,000	150,000	2.9
7	MBL/MAN	9/1	73	191	350	116,000	224,000	1.9
8	MBL/HEMA	9/1	96	194	370	120,400	436,300	3.6
9	MBL/MAAM	9/1	92	198	382	139,200	302,000	2.2

EXAMPLE 10

Preparation of a Three-Layer MBL Core/Shell Particle with no Styrene in the n-Butyl

Acrylate Layer to Match the Refractive Index

Step 1: Preparation of an MBL core

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 2.4L water, heated to 50°C, sparged with nitrogen for 30 min, and then allowed to cool to room temperature. A solution of MBL (110g), allyl methacrylate (2.8g), and DOS (1.0g) was added to the flask and

the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.121g) in 50mL water was added over 5 min. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky-white emulsion. The mixture was allowed to stir at 80°C for 1 hour and then sampled (approximately 1mL drawn out) for particle size measurement.

Step 2: Preparation of middle layer

A solution of potassium persulfate (0.27g) in 45mL water was added over 5 min to the milky-white emulsion obtained from step 1. A solution of n-butyl acrylate (250g), allyl methacrylate (6.4g), and DOS (2.3g) was added over 30 min and then held for 1 hour at 80°C. The mixture was sampled (approximately 1mL drawn out) for particle size measurement.

Step 3: Preparation of MBL shell

A solution of potassium persulfate (0.186g) in 33mL water was added over 5 min to the mixture obtained from step 2. A final charge of MBL (90g) was added over 30 min and then held for 1 hour at 80°C. The mixture was sampled (approximately 1mL drawn out) for particle size measurement. The emulsion was allowed to cool to room temperature and filtered through a course frit filter paper.

Step 4: Coagulation of MBL core/shell particle

The homopolymer emulsion (from example 1) was combined with the emulsion from step 3 above. The combined emulsion was added to 24L of water containing 240g MgSO₄ heated to 100°C. The polymer coagulates immediately and the slurry was brought back to reflux and held for one hour. After cooling, the solids were collected on a course frit filter and washed six times with 2L water each time, and dried to give 955g (95%) of the MBL core/shell particle mixed with MBL homopolymer as a white solid.

The coagulated polymer mixture from Example 10 was blended on a Prism[®] 16mm twin screw extruder at 270°C. The resulting pellets were injection molded on a 1.5 ounce injection molding machine in to ASTM D648 flex bars and ASTM D638 tensile bars.

TABLE 3

Blending	
Weight of coagulated polymer from example 10	955 g
Properties	
Flexural Strength (MPa)	48.3
Flexural Modulus (MPa)	2832
Tensile strength (MPa)	36.7
Tensile modulus (MPa)	3439
Elongation (%)	1.33
Notched Izod impact (J/m)	17.0
HDT (264 psi) (°C)	142

EXAMPLE 11

Preparation of a Three-Layer MBL-MMA Core/Shell Particle with Styrene in n-Butyl Acrylate Middle-Layer to Match the Refractive Index

Step 1: Preparation of MBL-MMA core

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 1.5L water, heated to 50°C, sparged with nitrogen for 30 min, and then allowed to cool to room temperature. A solution of MBL (68g), MMA (68g), ALMA (3.5g), and DOS (1.23g) was added to the flask and the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.141g) in 31mL water was added over 5 min. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky-white emulsion. The mixture was allowed to stir at 80°C for 1 hour and then sampled (approximately 1mL drawn out) for particle size measurement.

Step 2: Preparation of RI-matched rubbery middle-layer

A solution of potassium persulfate (0.36g) in 80mL water was added over 5 min to the milky-white emulsion obtained from step 1. A solution of butyl acrylate (176g), allyl methacrylate (9.0g), styrene (138g), and DOS(3.19g) was added over 30 min

and then held for 1 hour at 80°C. The mixture was sampled (approximately 1mL drawn out) for particle size measurement.

Step 3: Preparation of MBL-MMA shell

A solution of potassium persulfate (0.107g) in 19mL water was added over 5 min to the mixture of obtained as a result of step 2. A solution of MBL (52g), MMA (52g) was added over 30 min and then held for 1 hour at 80°C. The mixture was sampled (approximately 1mL drawn out) for particle size measurement.

Step 4: Coaquiation of MBL core/shell particle

The polymer emulsion (from Step 3) was allowed to cool to room temperature and filtered through course frit filter paper. The emulsion was coagulated with 9L of a 1% MgSO₄ solution at 40°C. The coagulated slurry was heated to 80°C to increase particle size and allow for faster filtration. The particles were collected on a course frit filter and washed three times with 2L of water each time, and dried to give 550g (97%) of the MBL core/shell particle as a white solid.

TABLE 4

Steps Particle Size in na		
	meter	
1	174	
2	228	
3	262	

EXAMPLE 12

Preparation of a Three-Layer MBL-MMA Core/Shell Particle without Styrene in the n-Butyl Acrylate Middle-Layer to Match the Refractive Index

Step 1: Preparation of an MBL-MMA core

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 2.0 L water, heated to 50°C, sparged with nitrogen for 30 min, and then allowed to cool to room temperature. A solution of MBL (68g), MMA (68g), allyl methacrylate (3.5g), and DOS (1.23g) was added and the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.141g) in 31mL water was added over 5 min. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky-

white emulsion. The mixture was allowed to stir at 80°C for 1 hour and then sampled (approximately 1mL drawn out) for particle size measurement.

Step 2: Preparation of middle layer

A solution of potassium persulfate (0.31g) in 80mL water was added over 5 min to the milky-white emulsion obtained from step 1. A solution of butyl acrylate (280g), allyl methacrylate (7.2g), and DOS(2.54g) was added over 30 min and then held for 1 hour at 80°C. The mixture was sampled (approximately 1mL drawn out) for particle size measurement.

Step 3: Preparation of MBL-MMA shell

A solution of potassium persulfate (0.107g) in 19mL water was added over 5 min to the mixture of obtained as a result of step 2. A solution of MBL (52g), MMA (52g) was added over 30 min and then held for 1 hour at 80°C. The mixture was sampled (approximately 1mL drawn out) for particle size measurement.

Step 4: Coagulation of MBL core/shell particle

The emulsion was coagulated with 9L of a 1% MgSO₄ solution at 40°C. The polymer coagulated immediately and the slurry was heated to 80°C to increase particle size and allow for faster filtration. The particles were collected on a course frit filter and washed three times with 2L of water each time, and dried to give 510g (96%) of the MBL core/shell particle as a white solid.

TABLE 5

Steps	Particle Size in nanome-		
	ter		
1	200		
2	289		
3	297		

EXAMPLE 13

Preparation of a Three-Layer MeMBL-MMA Core/Shell Particle with Styrene
in the n-Butyl Acrylate Layer

Step 1: Preparation of an MeMBL-MMA core

A 2L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 0.5L water, heated to 50°C, sparged

with nitrogen for 30 min, and then allowed to cool to room temperature. A solution of MeMBL (24g), MMA (8g), allyl methacrylate (0.8g), and DOS (0.29g) was added and the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.03g) in 10 mL water was added over 5 min. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky-white emulsion. The mixture was allowed to stir at 80°C for 1 hour and then sampled (approximately 1mL drawn out) for particle size measurement.

Step 2: Preparation of middle-layer with styrene in the n-butyl acrylate

A solution of potassium persulfate (0.083g) in 23mL water was added over 5 min to the milky-white emulsion obtained from step 1. A solution of n-butyl acrylate (50g), allyl methacrylate (1.9g), styrene (23g) and DOS (0.7g) was added over 30 min and then held for 1 hour at 80°C. The mixture was sampled (approximately 1 mL drawn out) for particle size measurement.

Step 3: Preparation of MeMBL-MMA shell

A solution of potassium persulfate (0.036g) in 6 mL water was added over 5 min to the mixture obtained in step 2. A solution of MeMBL (20g), MMA (6.6g) was added over 30 min and then held for 1 hour at 80°C. The mixture was sampled (approximately 1mL drawn out) for particle size measurement.

Step 4: Coagulation of MBL core/shell particle

The emulsion from step 3 was filtered and then added to a flask containing 2.5L water and 25g MgSO₄ at 50°C. The polymer coagulated immediately and the slurry was heated to 80°C to increase particle size and allow for faster filtration. The particles were collected on a course frit filter and washed three times with 2L of water each time, and dried to give 121g (90%) of the MeMBL core/shell particle as a white solid. A sample of the polymer was pressed at 260°C under 20,000 psi pressure to a thin, transparent film. A TEM analysis was performed on this sample, as shown in Figure 2.

TABLE 6

Steps	Particle Size in nano-	
	meter	
1	166	
2	211	
3	254	

EXAMPLE 14

<u>Preparation of a Three-Layer MeMBL-MMA Core/Shell Particle without Styrene in the n-Butyl Acrylate Middle-Layer to Match the Refractive Index</u>

Step 1: Preparation of an MeMBL-MMA core

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet is charged with 2.0 L water, heated to 50°C, sparged with nitrogen for 30 min, and then allowed to cool to room temperature. A solution of MeMBL (68g), MMA (68g), allyl methacrylate (3.5g), and DOS (1.23g) is added and the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.141g) in 31mL water is added over 5 min. Polymerization begins immediately and the mixture turns from a cloudy-clear emulsion to a milky-white emulsion. The mixture is allowed to stir at 80°C for 1 hour and then sampled (approximately 1mL drawn out) for particle size measurement.

Step 2: Preparation of middle layer

A solution of potassium persulfate (0.31g) in 80mL water is added over 5 min to the milky-white emulsion obtained from step 1. A solution of butyl acrylate (280g), allyl methacrylate (7.2g), and DOS(2.54g) is added over 30 min and then held for 1 hour at 80°C. The mixture is sampled (approximately 1mL drawn out) for particle size measurement.

Step 3: Preparation of MeMBL-MMA shell

A solution of potassium persulfate (0.107g) in 19mL water is added over 5 min to the mixture of obtained as a result of step 2. A solution of MeMBL (52g), MMA (52g) is added over 30 min and then held for 1 hour at 80°C. The mixture is sampled (approximately 1mL drawn out) for particle size measurement.

Step 4: Coagulation of MeMBL core/shell particle

The emulsion is coagulated with 9L of a 1% MgSO $_4$ solution at 40°C. The polymer coagulates immediately and the slurry is heated to 80°C to increase particle size and allow for faster filtration. The particles are collected on a course frit filter and washed three times with 2L of water each time, and dried to give 510g (96%) of the MeMBL core/shell particle as a white solid.

EXAMPLE 15

Preparation of a Cross-linked MBL Homopolymer Particle

Step 1: Preparation of an MBL seed particle

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 3L water, heated to 50°C, sparged with nitrogen for 30 minutes. A solution of MBL (97.5g), allyl methacrylate (2.5g), 1-dodecanethiol (0.2g), and DOS (2.5g) was added and the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.2g) in 10mL water was added all at once. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky-white emulsion. The mixture was allowed to stir at 80°C for 1 hour.

Step 2: Addition of more MBL monomer

A solution of potassium persulfate (0.6g) in 10mL water was added over 5 min to the milky white emulsion obtained from step 1. A solution of MBL (297g), DOS (7.5g), Alma (3g), and water (20mL) was added over 60 min and then held for 1 hour at 80°C.

Step 3: Coagulation of MBL particle

The emulsion from step 3 was filtered, sampled for particle size measurement, and then added to a flask containing 4.4L water and 44g MgSO₄ at 100°C. The polymer coagulated immediately and the slurry was heated back to 100°C to allow for faster filtration. The particles were collected on a course frit filter and washed with water (3 \times 2L) and dried to give 381g (95%) of the MBL particles as a white solid.

TABLE 7

Property	
T _g	195°C
T _d	380°C
Particle Size	302 nm

EXAMPLE 16

Preparation of a Cross-linked MeMBL Homopolymer Particle

Step 1: Preparation of an MeMBL seed particle

A 5 L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet is charged with 3 L water, heated to 50°C,

sparged with nitrogen for 30 minutes. A solution of MeMBL (97.5g), allyl methacrylate (2.5g), 1-dodecanethiol (0.2g), and DOS (2.5g) is added and the mixture is heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.2g) in 10mL water is added all at once. Polymerization begins immediately and the mixture turns from a cloudy-clear emulsion to a milky-white emulsion. The mixture is allowed to stir at 80°C for 1 hour.

Step 2: Addition of more MeMBL monomer

A solution of potassium persulfate (0.6g) in 10mL water is added over 5 min to the milky white emulsion obtained from step 1. A solution of MeMBL (297 g), DOS (7.5 g), Alma (3g), and water (20 mL) is added over 60 min and then held for 1 hour at 80°C.

Step 3: Coagulation of MeMBL particle

The emulsion from step 3 is filtered, sampled for particle size measurement, and then added to a flask containing 4.4 L water and 44 g MgSO₄ at 100° C. The polymer coagulates immediately and the slurry is heated back to 100° C to allow for faster filtration. The particles are collected on a course frit filter and washed with water (3 x 2L) and dried to give 381g (95%) of the MeMBL particles as a white solid.

EXAMPLE 17

Preparation of a Cross-linked MBL Particle containing Methacrylic Acid Step 1: Preparation of MBL seed particle

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 2.2L water, heated to 50°C, sparged with nitrogen for 30 min. A solution of MBL (100g), allyl methacrylate (2.8g), methacrylic acid (11.4g), and DOS (1.1g) was added and the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.11g) in 10mL water was added all at once. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky-white emulsion. The mixture was allowed to stir at 80°C for 1 hour.

Step 2: Addition of more MBL monomer

A solution of potassium persulfate (0.3g) in 10 mL water was added over 5 min to the milky white emulsion obtained from step 1. A solution of MBL (250g), DOS (2.8g),

Alma (7.1g), methacrylic acid (28g), and water (20mL) was added over 60 min and then held for 1 hour at 80°C.

Step 3: Coagulation of MBL particle

The emulsion from step 3 was filtered, sampled for particle size measurement, and then added to a flask containing 2L water and 20g MgSO₄ at 100°C. The polymer coagulated immediately and the slurry was heated back to 100°C to allow for faster filtration. The particles were collected on a course frit filter and washed three times with 2L water each time, and dried to give 319g (79%) of the MBL particles as a white solid.

TABLE 8

Property			
Tg	202°C		
Td	362°C		
Particle Size	505 nm		

EXAMPLE 18

Preparation of a Cross-linked MBL Particle containing Maleic Anhydride Step 1: Preparation of an MBL seed particle

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 2.7L water, heated to 50°C, sparged with nitrogen for 30 min. A solution of MBL (150g), allyl methacrylate (3.8g), and DOS (1.4g) was added and the mixture was heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.16g) in 10mL water was added all at once. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky white emulsion. The mixture was allowed to stir at 80°C for 1 hour.

Step 2: Addition of more MBL monomer

A solution of potassium persulfate (0.4g) in 10mL water was added over 5 min to the milky-white emulsion obtained from step 1. A solution of MBL (400g), DOS (3.6g), Alma (10.2g), maleic anhydride (4g), and water (150mL) was added over 60 min and then held for 1 hour at 80°C.

Step 3: Coagulation of MBL particle

The emulsion from step 3 was filtered, sampled for particle size measurement and isolated as above to give the polymer as a white solid.

TABLE 9

Property	
T _g	200°C
T _d	360°C
Particle Size	477 nm

EXAMPLE 19

<u>Preparation of a Cross-linked MeMBL Particle containing Methacrylic Acid</u> <u>Step 1: Preparation of MeMBL seed particle</u>

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet is charged with 2.2L water, heated to 50°C, sparged with nitrogen for 30 min. A solution of MeMBL (100g), allyl methacrylate (2.8g), methacrylic acid (11.4g), and DOS (1.1g) is added and the mixture is heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.11g) in 10mL water is added all at once. Polymerization begins immediately and the mixture turns from a cloudy-clear emulsion to a milky-white emulsion. The mixture is allowed to stir at 80°C for 1 hour.

Step 2: Addition of more MeMBL monomer

A solution of potassium persulfate (0.3 g) in 10 mL water is added over 5 min to the milky white emulsion obtained from step 1. A solution of MeMBL (250g), DOS (2.8g), Alma (7.1g), methacrylic acid (28g), and water (20 mL) is added over 60 min and then held for 1 hour at 80°C.

Step 3: Coagulation of MeMBL particle

The emulsion from step 3 is filtered, sampled for particle size measurement, and then added to a flask containing 2L water and 20g MgSO₄ at 100°C. The polymer coagulates immediately and the slurry is heated back to 100°C to allow for faster filtration. The particles are collected on a course frit filter and washed three times with 2L water each time, and dried to give 319g (79%) of the MeMBL particles as a white solid.

EXAMPLE 20

Preparation of a Cross-linked MeMBL Particle containing Maleic Anhydride

Step 1: Preparation of an MeMBL seed particle

A 5 L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet is charged with 2.7 L water, heated to 50°C, sparged with nitrogen for 30 min. A solution of MeMBL (150g), allyl methacrylate (3.8g), and DOS (1.4g) is added and the mixture is heated to 80°C while stirring at 200 rpm. A solution of potassium persulfate (0.16g) in 10mL water is added all at once. Polymerization begins immediately and the mixture turns from a cloudy-clear emulsion to a milky white emulsion. The mixture is allowed to stir at 80°C for 1 hour. Step 2: Addition of more MeMBL monomer

A solution of potassium persulfate (0.4g) in 10mL water is added over 5 min to the milky-white emulsion obtained from step 1. A solution of MeMBL (400g), DOS (3.6g), Alma (10.2g), maleic anhydride (4g), and water (150mL) is added over 60 min and then held for 1 hour at 80°C.

Step 3: Coagulation of MeMBL particle

The emulsion from step 3 is filtered, sampled for particle size measurement and isolated as above to give the polymer as a white solid.

EXAMPLE 21

Preparation of a 25/75 MeMBL-MMA Copolymer

Using the general procedure described in Example 2, a 25/75 MeMBL-MMA copolymer was prepared. The polymer had a Tg of 130°C, Td 342°C, Mn 56,400, Mw 110,000, PDI 1.95.

EXAMPLE 22

Preparation of a Two-Layer NBA/Styrene // MeMBL/MMA Core//Shell Particle for Toughening a 25/75 MeMBL-MMA Resin

Step 1: Preparation of an Butyl Acrylate/Styrene core

A 5 L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 1.4 L water and heated to 80°C while sparging with nitrogen. A solution of NBA (138 g), allyl methacrylate (4.8 g), styrene (54g) and DOS (1.9 g) was prepared and 20 mL of this solution was

added to the flask while stirring at 200 rpm. A solution of potassium persulfate (0.38 g) in 50 mL water was added over 5 min. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky-white emulsion. The remainder of the monomer solution was added over 30 min. The mixture was then allowed to stir at 80°C for 1.5 hours and then sampled (approximately 1 mL drawn out) for particle size measurement. Particle size was 221 nm by light scattering measurement.

Step 2: Preparation of MeMBL/MMA shell

A solution of potassium persulfate (0.096 g) in 33mL water was added over 5 min to the emulsion obtained from step 1. A solution of MeMBL (12 g), MMA (36 g), DOS (0.48 g), and EHT (0.48 g) was added over 1 hour and then held for 1 hour at 80°C. The emulsion was allowed to cool to room temperature and filtered through a course frit filter paper. Particle size was 257 nm by light scattering measurement. Step 3: Coagulation of NBA/Styrene // MeMBL/MMA core//shell particle

The polymer emulsion (from Step 2) was coagulated with 2 L of a 1% MgSO₄ solution at 40°C. The particles were collected on a course frit filter and washed three times with 2L of water each time, and dried to give 237 g of the core/shell particle as a white solid.

EXAMPLE 23-24

Mixing the NBA/Styrene//MeMBL/MMA Core//Shell Toughener with a MeMBL-MMA Copolymer

A 25/75 MeMBL-MMA copolymer (made as illustrated in example 17), was mixed with the core/shell toughener (made as illustrated in example 18) in a Prism[®] 16 mm, twin-screw extruder at 250°C. The resulting pellets were injection molded on a 1.5 ounce injection molding machine in to ASTM D648 flex bars and ASTM D638 tensile bars. The test specimens were transparent had a good balance of HDT and toughness, as shown in the table below.

TABLE 10

Example No.	23	24
Extrusion	Blending	
Polymer From Example 17	450	350
Core/shell particle from Example 18 (g)	150	250
Weight % core/shell particle	25	42
Injection Molding and Physical Testing		
Flexural Modulus (MPa)	2535	1764
Tensile strength (MPa)	50	37
Elongation (%)	4.3	19.3
Notched-Izod impact (J/m)	20	46
HDT (264 psi) (°C)	87	80

EXAMPLES 25-27

Mixing the MBL-MMA Copolymer with Core/Shell Tougheners

MBL-MMA copolymers (made as illustrated in example 1), were mixed with core/shell tougheners (made as illustrated in example 2 and example 3) in a Prism[®] 16mm twin-screw extruder at 240°C. The resulting pellets were injection molded on a 1.5 ounce injection molding machine in to ASTM D648 flex bars and ASTM D638 tensile bars.

TABLE 10

Example No.	25	26	27		
Example ite:	Extrusion Blending				
Polymer From Example 1	530	530	549		
(g) Core/shell particle from Example 11, (g)	201	350	-		
Core/shell particle from Example 12, (g)	-	-	509		
Weight % core/shell parti-	27	40	48		
Extrusion temperature °C	250	250	250		
Annearance	transparent	transparent	opaque white		
Injection Molding and Physical Testing					
Flexural Strength (MPa)	67.4	54.8	46.0		
Flexural Modulus (MPa)	3576	2894	2439		
Flexural Modulus (Mr a)	43.8	44.2	42.9		
Tensile strength (MPa)	2260	2109	2315		
Tensile modulus (MPa)	2.4	3.6	2.7		
Elongation (%)	11.2	11.7	19.9		
Notched-Izod impact (J/m)	108.9	106.6	107.6		
HDT (264 psi) (°C)	100.9	1.00.0	1		

EXAMPLE 28

Synthesis of a MBL-Glycidyl Methacrylate-Copolymer via Low-Temperature Emulsion Polymerization using a Redox -type Initiator System

Step 1: Preparation of an MBL-GMA seed emulsion

A 5L, 4-neck, round bottom flask equipped with a mechanical stirrer, addition funnel, condenser, and nitrogen inlet was charged with 1.8L water and sparged with nitrogen at room temp. for 30 min. To this was added MBL (45g), glycidyl methacrylate (5g), DOS (0.5g), sodium formaldehyde sulfoxylate dihydrate (0.3g), and ethylhexylthioglycolate (0.15g) with stirring at 200 rpm. A stock solution of EDTA tetrasodium salt hydrate (3g), Iron sulfate heptahydrate (2g), and water (100g) was prepared and 1.2mL of this solution was added to the monomer emulsion. A solution of t-butyl hydroperoxide (0.3g, 0.46 mL of a 70% solution in water) was added all at once. Polymerization began immediately and the mixture turned from a cloudy-clear emulsion to a milky-white emulsion. The mixture was allowed to stir at room temperature for 1 hour.

Step 2: Addition of more monomer

A solution of t-butyl hydroperoxide (1.2g, 1/8mL of a 70% solution in water) in 10mL water was added all at once. A solution of MBL (180g), GMA (20g), DOS (2g), so-dium formaldehyde sulfoxylate dihydrate (1.2g), EHT (0.6g) and 10mL water was added over 60 min and then held for 1 hour at room temp. The temperature rose from 21°C to 32°C during the course of the polymerization.

Step 3: Freeze drying the copolymer emulsion

The polymer emulsion was freeze dried to give 253g dried polymer.

TABLE 11

Property	
T _g	185°C
T _d	361°C
Mn	85,200
Mw	221,000
PD	2.6

EXAMPLES 29-32

Nylon Blends and Nylon Control

The polymers from examples 25-27 were blended on a Prism® 16mm, twin screw extruder at 280°C with Nylon 6,6 (Zytel 101®). The resulting pellets were injection molded on a 1.5 ounce injection molding machine in to ASTM D648 flex bars and ASTM D638 tensile bars.

TABLE 14

The second of th			
Example	Blend Composition	HDT@264 psi (°C)	Flex Modulus (MPa)
No. 29	Zytel®101 control	71	2832
30	Polymer from Example 14, 40% Zytel® 101, 60% cross-linked MBL homopolymer	118	2680
31	Polymer from Example 15, 40% Zytel® 101, 60% cross-linked MBL polymer with methacrylic acid	108	3804
32	Polymer from Example 16, 40% Zytel® 101, 60% cross-linked MBL with maleic anhydride	112	3046

CLAIMS

What is claimed is:

 An acrylic copolymer comprising at least a first polymeric repeat unit represented by Formula I, derived from α-methylene lact(one)(am) monomer,

$$H_2C$$
 R^1
 R^2
 R^3
 R^4
 R^6

wherein:

n is 0, 1 or 2;

X is -O- or -NR9-; and

R¹, R², R⁵, R⁶, R⁹, each of R³, and each of R⁴, are independently hydrogen, a functional group, hydrocarbyl or substituted hydrocarbyl.

- 2. The acrylic copolymer of Claim 1, further comprising at least one additional polymer or copolymer.
- 3. The acrylic copolymer of Claim 1, wherein the copolymer comprises a core, the core being optionally cross-linked, and at least one shell, the shell being optionally cross-linked, wherein the core and the shell are prepared from a polymer selected from the group consisting of:
 - (a) a polymer or a copolymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula II,
 - (b) a polymer or a copolymer derived from at least one other freeradically polymerizable monomer,
 - (c) a copolymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula II and at least one other free-radically copolymerizable monomer,

$$H_2C$$
 R^1
 R^2
 R^3
 R^4
 R^5
(II)

wherein:

n is 0, 1 or 2;

X is -O- or -NR9-; and

R¹, R², R⁵, R⁶, R⁹, each of R³, and each of R⁴, are independently hydrogen, a functional group, hydrocarbyl or substituted hydrocarbyl.

- (d) an optionally cross-linked polymer derived from at least one conjugated diolefin monomer,
- (e) an optionally cross-linked polymer derived from at least one vinyl monomer, and
 - (f) an optionally cross-linked polymer derived from at least one conjugated diolefin monomer and one vinyl monomer.
- 4. The acrylic copolymer of Claim 3, which comprises:
 - (i) from about 1 to about 99 parts by weight of a core polymer,
 - (ii) from about 0 to about 99 parts by weight of at least one intermediate shell polymer, and
 - (iii) from about 1 to about 99 parts by weight of outer shell polymer.
- 5. The acrylic copolymer of Claim 4, wherein the intermediate shell is prepared from a polymer selected from the group consisting of:
 - (a) a polymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula I,
 - (b) a polymer derived from at least one free radically polymerizable monomer,

- (c) a polymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula I and at least one other free radically polymerizable monomer,
- (d) an optionally cross-linked polymer derived from at least one conjugated diolefin monomer,
- (e) an optionally cross-linked polymer derived from at least one vinyl monomer, and
- (f) an optionally cross-linked polymer derived from at least one conjugated diolefin monomer and one vinyl monomer.
- 6. The acrylic copolymer of Claim 4, wherein the core polymer, the intermediate shell polymer and the outer shell polymer, independently are selected from polymers of α-methylene-γ-butyrolactone of Formula (III), γ-methyl-αmethylene-γ-butyrolactone of Formula (III), and at least one other monomer capable of being polymerized by free radical polymerization

$$CH_2$$
 CH_3
 CH_3
 (IV)

- 7. The acrylic copolymer of Claim 5, wherein the intermediate shell has a glass transition temperature of -125°C to 25°C.
- 8. A process for producing an acrylic copolymer comprising the sequential steps of:
 - (a) graft polymerizing α -methylene- γ -butyrolactone or γ -methyl- α -methylene- γ -butyrolactone onto a polymerized butadiene or butadiene-copolymer to form a latex, and
 - (b) isolating the resulting latex by coagulation, freeze drying, or spray drying.

9. A process for producing a cross-linked α -methylene- γ -butyrolactone or γ -methyl- α -methylene- γ -butyrolactone copolymer, the method comprising emulsion polymerizing α -methylene- γ -butyrolactone or γ -methylene- γ -butyrolactone.

- 10. A method of polymerizing at least one monomer of Formula (I), comprising the steps:
 - (a) contacting said monomer in an aqueous medium with a chaintransfer agent and a surfactant,
 - (b) adding an initiator to the product of step (a) to produce a polymer emulsion, and
 - (c) coagulating the polymer emulsion produced in step (b) to obtain a polymer product.
- 11. A method of copolymerizing at least one monomer of Formula (I) with at least one other free radically polymerizable monomer, the method comprising,
 - (a) contacting the monomers in an aqueous medium with a chaintransfer agent and a surfactant,
 - (b) adding an initiator to the product of step (a) to produce a polymer emulsion, and
 - (c) coagulating the polymer emulsion of step (b) to obtain the polymer product.
- 12. The method of Claim 10, wherein the monomer is α -methylene- γ -butyrolactone of Formula (II).
- 13. The method of Claim 10, wherein the monomer is γ -methyl- α -methylene- γ -butyrolactone of Formula (III).
- 14. The method of Claim 11, wherein the monomers are α -methylene- γ -butyrolactone of the Formula (II) and methyl methacrylate.

 The method of Claim 11, wherein the monomers are α-methylene-γbutyrolactone of Formula (II) and vinyl chloride.

- 16. The method of Claim 10, wherein the monomers are α -methylene- γ -butyrolactone of Formula (II) and γ -methyl- α -methylene- γ -butyrolactone of Formula (III).
- 17. The method as recited in Claims 12, 13, 14, 15, or 16, wherein the chain transfer agent is 2-ethylhexylthioglycolate, the surfactant is dioctylsulfosuccinate, the initiator is potassium persulfate, and the coagulant is MgSO₄.
- 18. The method of Claim 10 or Claim 11, wherein the chain transfer agent is selected from a group consisting of mercaptans, polymercaptans, and polyhalogen compounds.
- 19. The method of Claim 10 or Claim 11, wherein the surfactant is selected from a group consisting of alkali metals and ammonium salts of alkyl, aryl, alkaryl, and ara-alkyl sulfonates, sulfates, and polyether sulfates, ethoxylated fatty acids, esters, alcohols, amines, amides, alkyl phenols, complex organophosphoric acids, and their alkali metal and ammonium salts.
- 20. The method of Claim 10 or Claim 11, wherein the initiator is selected from the group consisting of thermal initiators, azo-type initiators, persulfates, peroxysulfates, and redox-type initiators.
- 21. The method of Claim 20 wherein the thermal initiators are selected from the group consisting of organo peroxides, acetyl peroxides, lauroyl peroxide, t-butyl peroxide, di-t-butyl hydroperoxide, and peresters; and the redox-type initiators are selected from the group consisting of hydroperoxide being selected from the group consisting of hydrogen peroxide, t-butyl hydroperoxide, cumene hydroperoxide, and diisopropyl-benzene hydroperoxide, and a reducing agent being selected from the group consisting

of sodium, potassium, or ammonium bisulfite, metabisulfite, hydrosulfite, sulfur dioxide, hydrazine, ferrous salts, isoascorbic acid, and sodium formaldehyde sulfoxalate.

- 22. The method of Claim 10 or Claim 11, wherein the coagulant is selected from a group consisting of magnesium sulfate, sodium chloride, and calcium chloride.
- 23. A method of polymerizing at least one monomer of Formula (I), comprising the sequential steps of,
 - (a) contacting the monomer in an aqueous medium with a chaintransfer agent and a surfactant in a reaction vessel,
 - (b) agitating the contents of the reaction vessel,
 - (c) adding an initiator to the reaction vessel to produce a polymer emulsion,
 - (d) coagulating the polymer emulsion by contacting with a solution of MgSO₄ held at about 60-100°C to produce a polymer product,
 - (e) filtering the coagulated polymer product through a filter,
 - (f) optionally washing the polymer, and
 - (g) optionally drying the polymer.
- 24. A thermoplastic polymer composition comprising one or more thermoplastic polymers and from about 1 percent by weight to about 80 percent by weight of the acrylic copolymer of Claim 3, based on total weight of the thermoplastic polymer and the acrylic copolymer.
- 25. The composition of recited in Claim 24, wherein the multi-stage acrylic polymer comprises:
 - (a) a core prepared from an optionally cross-linked polymer selected from:
 - (i) a polymer derived from at least one α -methylene lact(one)(am) monomer of Formula I,
 - (ii) a polymer derived from at least one other free radically polymerizable monomer, and

(iii) a polymer derived from at least one α-methylenelact(one)(am) monomer of Formula I and at least one other free radically polymerizable monomer; and

- (b) at least one shell made from optionally cross-linked polymer selected from:
 - (i) a polymer derived from at least one α -methylene lact(one)(am) monomer represented by Formula I,
 - (ii) a polymer derived from at least one other free radically polymerizable monomer, and
 - (iii) a polymer derived from at least one α-methylene lact(one)(am) monomer of Formula I and at least one other free radically polymerizable monomer.
- 26. The composition of Claim 25, wherein the multi-stage acrylic polymer comprises repeat units of a free radically polymerizable monomer.
- 27. The composition of Claim 24, wherein the first polymeric repeat unit of the multi-stage acrylic polymer is α–methylene-γ-butyrolactone of Formula (II).
- 28. The composition of Claim 24, wherein the first polymeric repeat unit of the multi-stage acrylic polymer is methyl-methylene-γ-butyrolactone of Formula (III).
- 29. The composition as recited in Claims 24, 25, 26, 27, or 28, wherein the thermoplastic polymer is selected from the group consisting of polymers derived from at least one α-methylene lact(one)(am) monomer of Formula I; polymers derived from at least one other free radically polymerizable monomer; polymers derived from at least one α-methylene lact(one)(am) monomer of Formula I and at least one other free radically polymerizable monomer; polyamides; polyesters; polycarbonates; polyethers; poly(vinyl)chlorides; polyolefins; polystyrenes; polyacetals; acrylonitrile/butadiene/styrene resins; and combinations thereof.

30. The composition of Claim 29, wherein R¹, R², R³, R⁴, R⁵ and R⁶ are all independently hydrogen or alkyl containing 1 to 6 carbon atoms, and X is -O-.

- 31. The composition of Claim 30 wherein n is 0.
- 32. The composition of Claim 31 wherein R¹, R², R³, R⁴, R⁵ and R⁶ are all hydrogen.
- 33. The composition of Claim 29 wherein the free radically copolymerizable monomers are derived from one or more of

$$R^{16}$$
 R^{16}
 R^{17}
 R^{18}
 R^{10}
 R^{10}

wherein R¹⁴ is hydrogen or methyl, R¹⁵ is hydrocarbyl or substituted hydrocarbyl, and R¹⁶ is hydrogen or methyl, and R¹⁷, R¹⁸, R¹⁹, R²⁰ and R²¹ are each independently hydrogen, hydrocarbyl substituted hydrocarbyl or a functional group.

34. The composition of Claim 24 wherein the free radically copolymerizable monomer is derived from one or more of

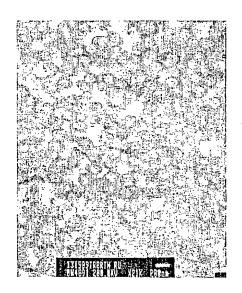
$$R^{16}$$
 R^{14}
 R^{16}
 R^{17}
 R^{17}
 R^{18}
 R^{19}
 R^{18}
 R^{19}
 R^{19}
 R^{19}

wherein R^{14} is hydrogen or methyl, R^{15} is hydrocarbyl or substituted hydrocarbyl, and R^{16} is hydrogen or methyl, and R^{17} , R^{18} , R^{19} , R^{20} and R^{21} are

each independently hydrogen, hydrocarbyl substituted hydrocarbyl or a functional group.

- 35. The composition of Claim 29 wherein the free radically copolymerizable monomer is derived from methyl methacrylate and optionally other copolymerizable monomers.
- 36. The composition of Claim 29 wherein the free radically copolymerizable monomer is derived from vinyl chloride.

FIGURE 1



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FIGURE 2

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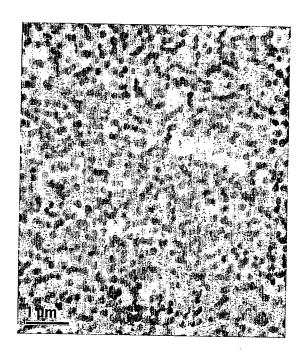
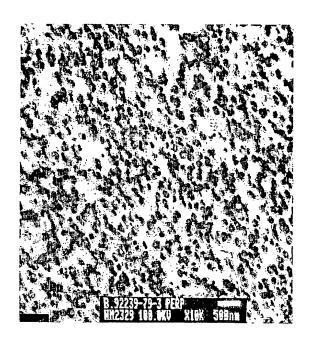


FIGURE 3



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(54) Title: GRAFT COPOLYMERS OF METHYLENE LACTONES AND PROCESS FOR EMULSION POLYMERIZATION OF METHYLENE LACTONES

(57) Abstract: This invention discloses resilient, acrylic graft polymers comprising α -methylene lact(one)(am) monomers such as α -methylene- γ -butyrolactone, and blends of such polymers with thermoplastic matrix resins. This invention also discloses hard, non-resilient, acrylic graft polymers comprising α -methylene lact(one)(am) monomers such as α -methylene- γ -butyrolactone, and to blends of such polymers with thermoplastic matrix resins. This invention further discloses a general process for emulsion polymerization of α -methylene lact(one)(am) monomers such as α -methylene- γ -butyrolactone and its copolymers.

INTERNATIONAL SEARCH REPORT

PCT/US 02/38338

A C: 4 C:	A CLASSIFICATION OF SUBJECT MATERS						
IPC 7	FICATION OF SUBJECT MATTER C08F220/12 C08F291/00 C08F22 C08L37/00 C08L51/00	4/00 C08F269/	00 Ć08L	57,00			
According to International Patent Classification (IPC) or to both national classification and IPC							
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Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched							
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C. DOCUMENTS CONSIDERED TO BE RELEVANT							
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Α	WO 01 64793 A (E.I. DU PONT DE 1 7 September 2001 (2001-09-07)	NEMOURS)		1			
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